

# AlSiC Replacement for Copper and Aluminum Baseplates

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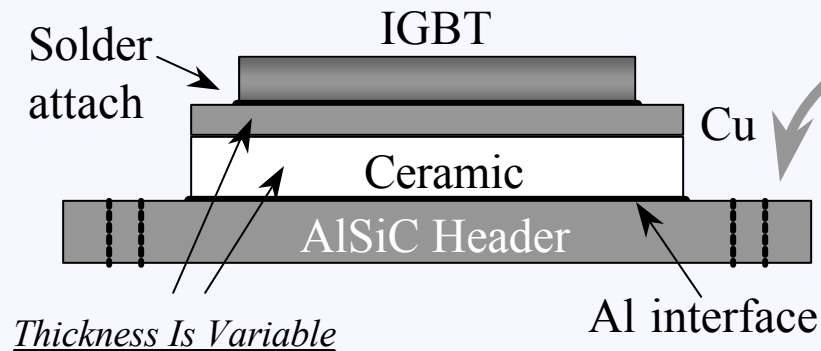
*see also*

“Thermal Impedance and Stress in a Power Package Due to Variations in Layer Thickness”

Acknowledgments: J. M. Pitarresi and J. A. Karker

# Direct Attached Ceramic on AlSiC

## Ceramic on AlSiC

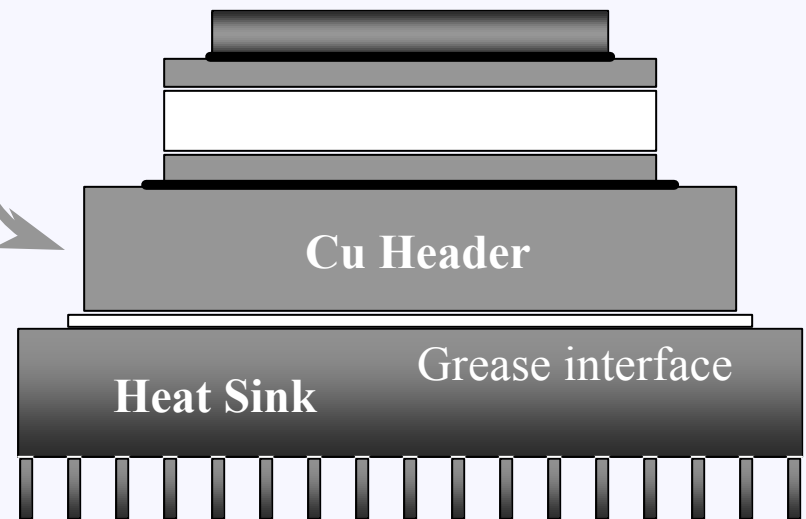


Layer	TCE	Modulus	Density
AlSiC	7.2	226	2.94
Cu	17.3	126	8.96

## Process:

1. DBC on ceramic
2. During Al impregnation of SiC (-600°C) the ceramic wets and is attached. Cu anneals.
3. IGBT is attached.

## Conventional Package



# AlSiC Replacement

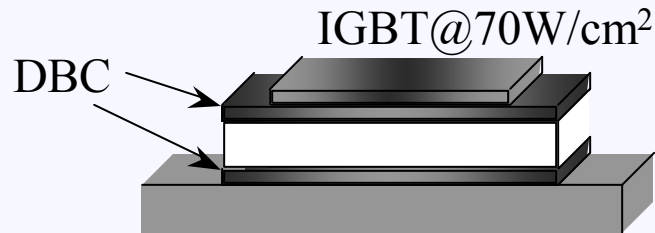
Maintain same plate bending rigidity:

$$\begin{aligned} \text{Thickness:} & \quad \alpha = t_{\text{AlSiC}} / t_o \\ \text{Weight:} & \quad \beta = w_{\text{AlSiC}} / w_o \\ \text{Thermal Resist.:} & \quad \gamma = R_{\theta, \text{AlSiC}} / R_{\theta, o} \end{aligned}$$

Replacing	$\alpha$	$\beta$	$\gamma$
Aluminum	0.69	0.75	0.97
Copper	0.80	0.26	1.85

# Thermal Spreading

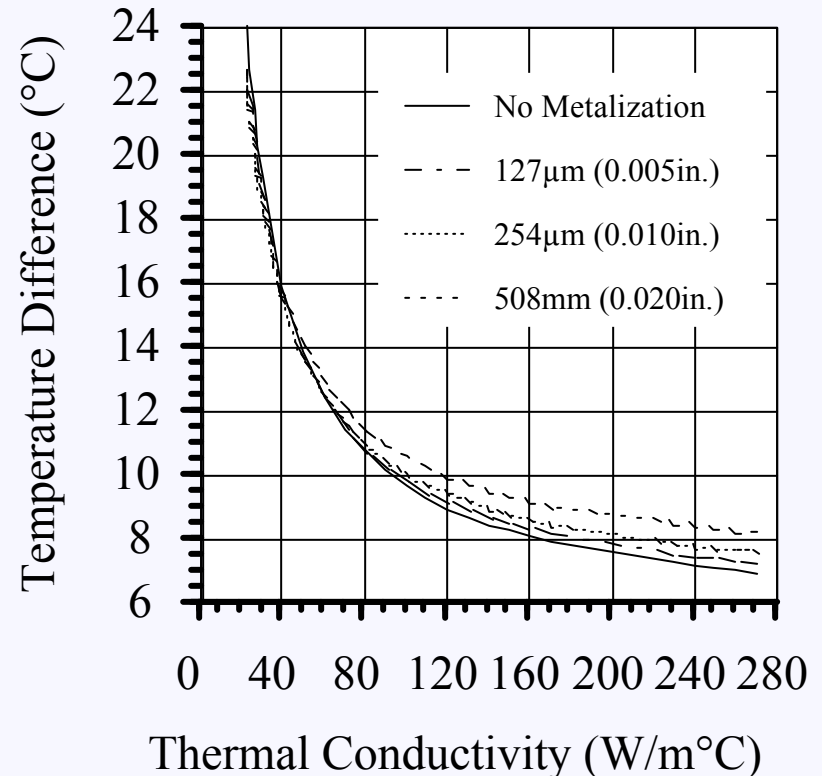
- Previous Work



- 635 $\mu$ m (25mils) Ceramic
- Vary Cu thickness

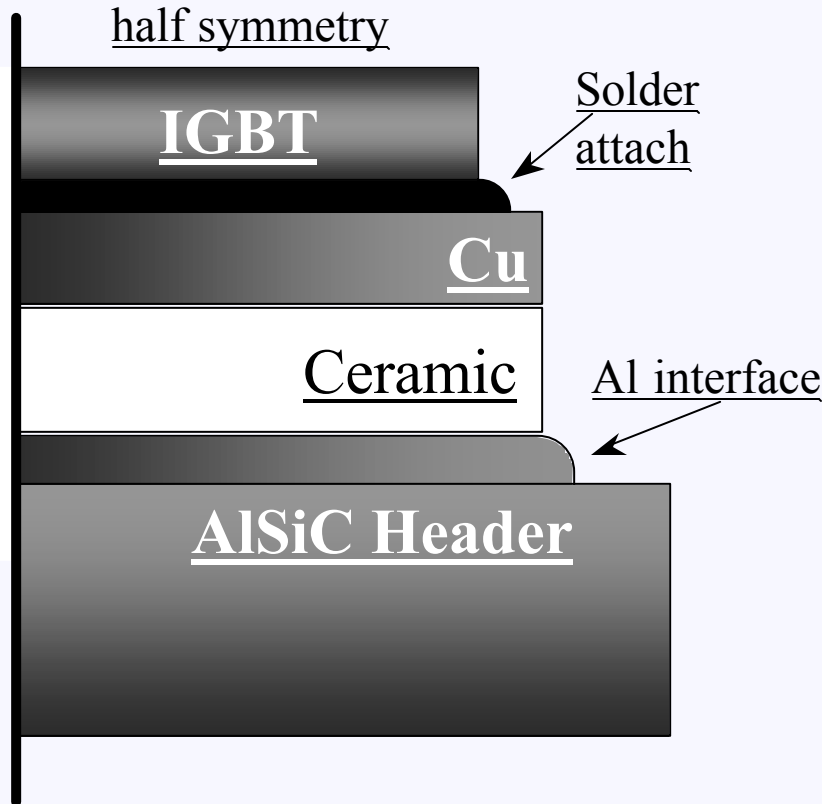
- Results

- Optimum Cu thickness on Al<sub>2</sub>O<sub>3</sub> (of 285 $\mu$ m).
- Increasing Cu thickness increases thermal conductance on BeO, AlN



# Physical Performance

- Module Structure



- Variables:

copper thickness: 75–510 $\mu\text{m}$   
 ceramic thickness: 75–635 $\mu\text{m}$   
 ceramic type:  $\text{Al}_2\text{O}_3$ , AlN, BeO  
 AlSiC: 1.3–6.4mm

Layer	Thickness ( $\mu\text{m}$ )	Width/2 (mm)
Silicon	350	5.1
63Sn/37Pb	101	5.59
Copper	75-510	6.6
Ceramic	75-635	7.1
Al (356)	51	17.1
AlSiC	1.3-6.4mm	18.4
Adhesive	51	8.4
Baseplate	13.2mm	10.9

# Finite Element Analysis

- Dual models:  
thermal and stress,  
with 8-node solid elements
- Meshed for  $< 5\%$  error
- IGBT with  $200\text{W}/\text{cm}^2$
- $25^\circ\text{C}$  thermal ground
- $125^\circ\text{C}$  max at IGBT
- Linear model with no pre-stress.

- Cases Studied

	Layer Thickness		
	Ceramic	Copper	AlSiC
Case I	<i>varied</i>	203 $\mu\text{m}$	635 $\mu\text{m}$
Case II	76 $\mu\text{m}$	<i>varied</i>	635 $\mu\text{m}$
Case III	254 $\mu\text{m}$	203 $\mu\text{m}$	<i>varied</i>

- Stress bounds:

Copper 192 MPa (equivalent stress)

Ceramic 264 MPa (tensile principle)

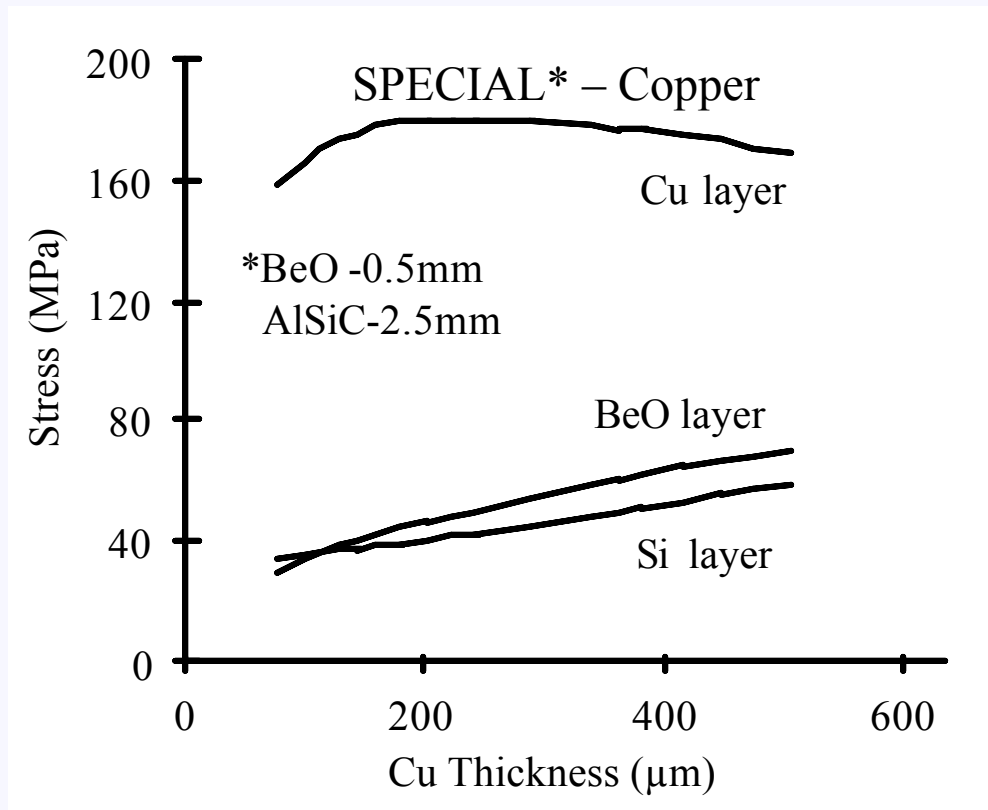
Silicon 128 MPa (tensile principle)

# Results - optimum thickness

- Special Case

Ceramic	Copper	AlSiC
0.5mm	<i>varied</i>	635 $\mu$ m
BeO		

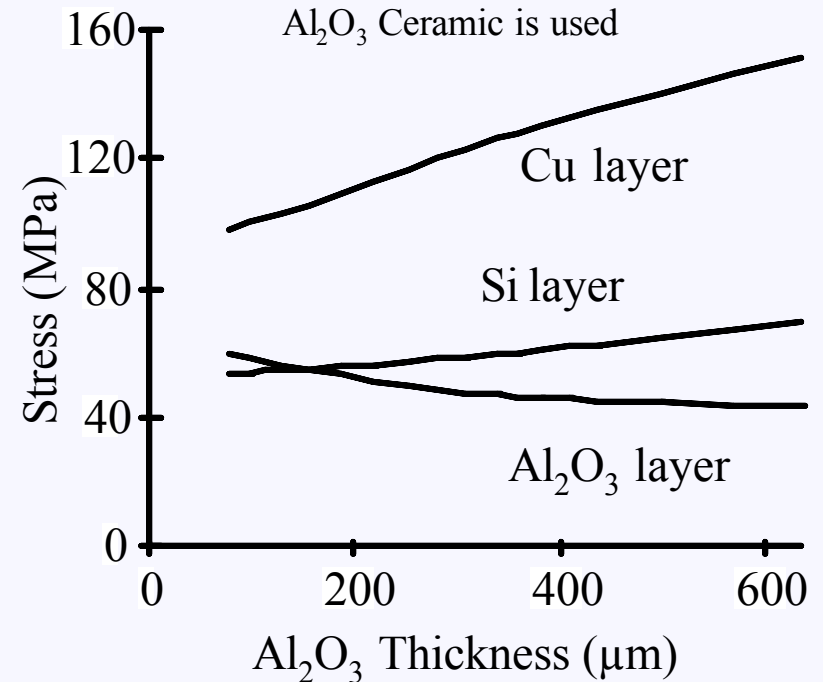
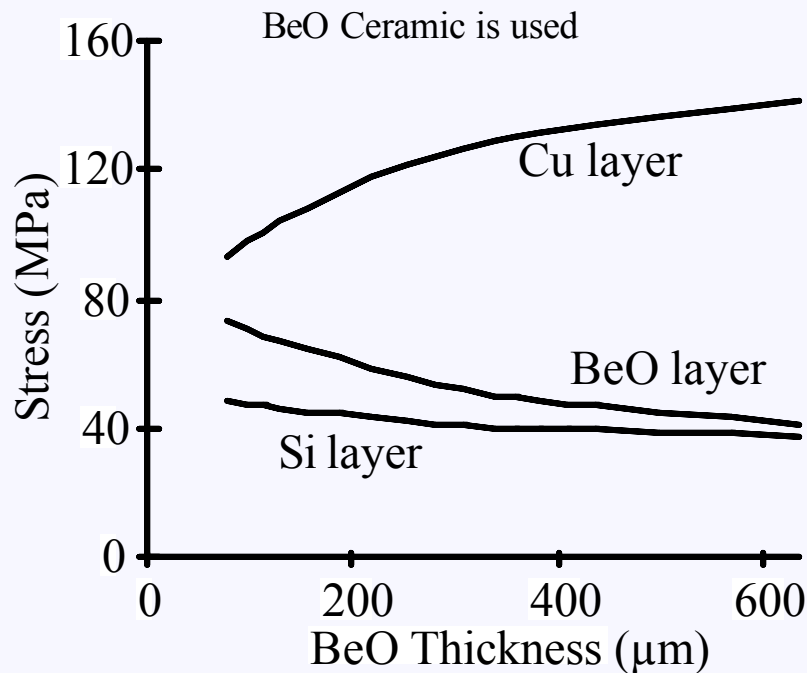
– Example of thickness extremum that maximizes stress. Similar to optimum thickness for thermal conductance.



# Results - variable ceramic thickness

- Case I – Stress

Ceramic	Copper	AlSiC
<i>varied</i>	203 $\mu\text{m}$	635 $\mu\text{m}$



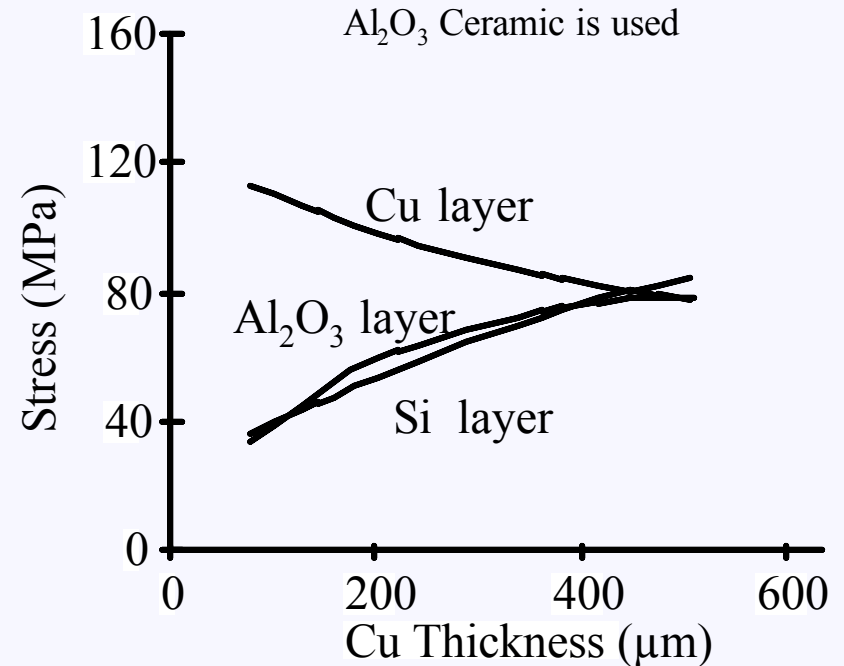
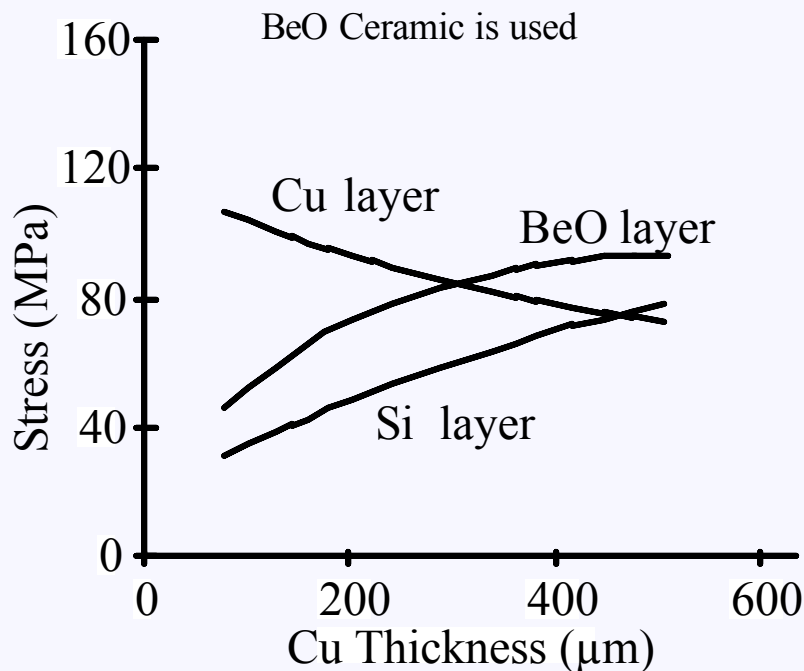
- Si on BeO has lower stress due to lower  $\delta T^\circ$ .
- Thinner ceramic has higher stress for this Cu thickness.



# Results - variable copper thickness

- Case II – Stress

Ceramic	Copper	AlSiC
76 $\mu\text{m}$	<i>varied</i>	635 $\mu\text{m}$

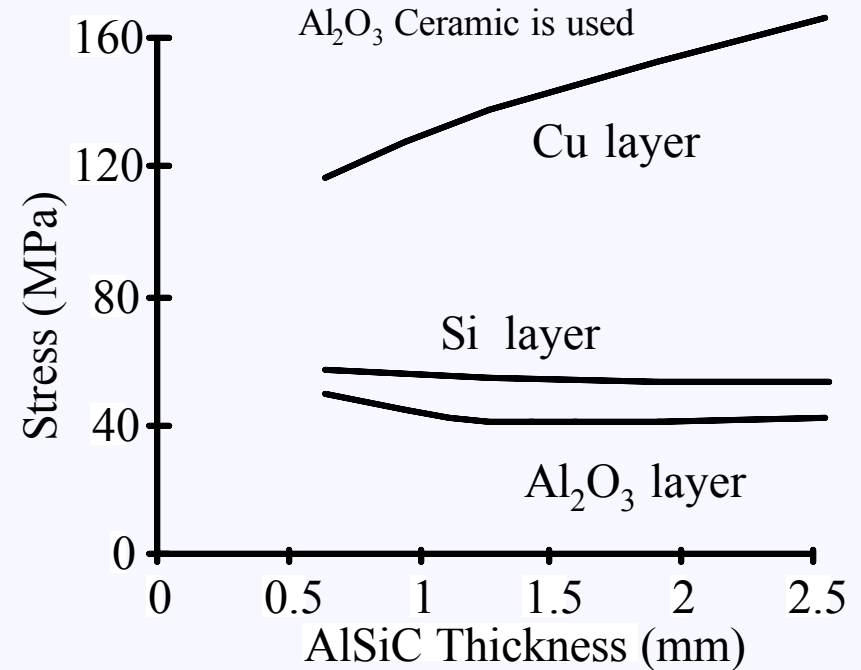
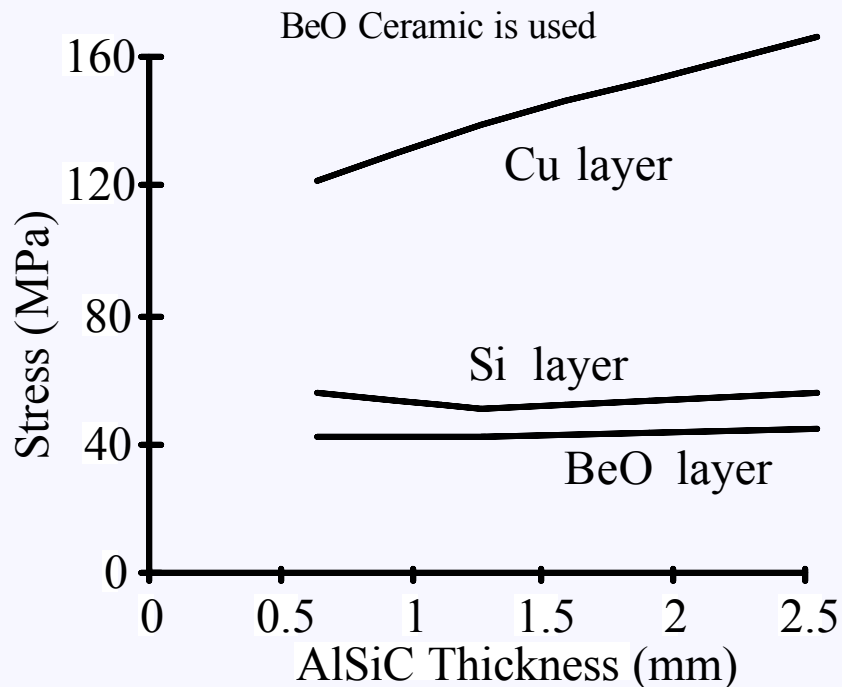


- Thinner copper relieves the stress in the ceramic and Si.
- Thinner Cu has higher stress.

# Results - variable AlSiC thickness

- Case III – Stress

Ceramic	Copper	AlSiC
254 $\mu\text{m}$	203 $\mu\text{m}$	<i>varied</i>



- Extremums in both Si and Al<sub>2</sub>O<sub>3</sub> are observed.
- The matched TCE of AlSiC and ceramic minimizes the ceramic and Si stress.
- Cu reacts to TCE mismatch.

# Summary

- Direct-attached-ceramic on AlSiC reduces the number of package layers – reducing the thermal impedance and stress. The TCE of AlSiC is 7.2 and ceramic is 5.8 to 7.4.
- FEM analysis used to evaluate thermal conductance and thermally induced stress for various Cu, *ceramic* and AlSiC layer thicknesses.
- Generally, thinner layers provide less stress due to lower thermal gradients.